

A two-level nonlinear beam model using adjoints

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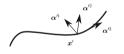
Politecnico di Milano

FEniCS 2021, March 22-26

Introduction

Beam model

- Domain: line
- Unknowns: \pmb{x}' , $\pmb{\alpha}'$
- Needs constitutive law $\{ {m T}, {m M} \} (\epsilon, eta)$



Handling of finite rotations in Dolfin, proc. FEniCS Conference 2017

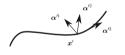
https://home.aero.polimi.it/morandini/Downloads/DolfinFiniteRotations/html/



Introduction

Beam model

- Domain: line
- Unknowns: \mathbf{x}' , $\mathbf{\alpha}'$
- Needs constitutive law $\{\mathbf{T}, \mathbf{M}\}(\epsilon, \beta)$



Cross-section models

- Domain: cross section (area)
- Unknowns: $\hat{\boldsymbol{u}}_i$
- Known 3D constitutive law
- Function of {*T*, *M*} (forcing term)



Handling of finite rotations in Dolfin, proc. FEniCS Conference 2017

 $\label{eq:https://home.aero.polimi.it/morandini/Downloads/DolfinFiniteRotations/html/$

Analysis of beam cross section response accounting for large strains and plasticity, IJSS, 2019.



Beam model: from $\{x', \alpha'\}$

$$\int_{L} \left(\delta \boldsymbol{\varepsilon} \, \boldsymbol{T} + \delta \boldsymbol{\beta} \, \boldsymbol{M} \right) \mathrm{d} \boldsymbol{s} - \delta L_{\boldsymbol{e}} = \boldsymbol{0}$$



Beam model: from {**x**', **α**'}

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to $\{ \pmb{x}', \pmb{lpha}', \pmb{T}, \pmb{M} \}$



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to $\{ \pmb{x}', \pmb{lpha}', \pmb{T}, \pmb{M} \}$

complementary strain energy

$$v(T, M) = \epsilon T + \beta M - w(\epsilon, \beta)$$



Beam model:
 from {*x*', *α*'}

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complementary strain energy

$$v(\mathbf{T}, \mathbf{M}) = \epsilon \mathbf{T} + eta \mathbf{M} - w(\epsilon, eta)$$

$$\mathcal{H}(\delta\{\boldsymbol{\epsilon},\boldsymbol{\beta},\boldsymbol{T},\boldsymbol{M}\},\{\boldsymbol{\epsilon},\boldsymbol{\beta},\boldsymbol{T},\boldsymbol{M}\}) = \int_{I} (\delta\boldsymbol{\epsilon}\boldsymbol{T} + \delta\boldsymbol{\beta}\boldsymbol{M} + \delta\boldsymbol{T}\boldsymbol{\epsilon} + \delta\boldsymbol{M}\boldsymbol{\beta} - \delta\boldsymbol{v}) \,\mathrm{d}\boldsymbol{s} - \delta\boldsymbol{L}_{\boldsymbol{e}} = 0$$



Beam model:
 from {*x*', *α*'}

$$\int_{L} \left(\delta \boldsymbol{\varepsilon} \, \boldsymbol{T} + \delta \boldsymbol{\beta} \, \boldsymbol{M} \right) \mathrm{d} \boldsymbol{s} - \delta L_{\boldsymbol{e}} = \boldsymbol{0}$$

to $\{ \pmb{x}', \pmb{lpha}', \pmb{T}, \pmb{M} \}$

complementary strain energy

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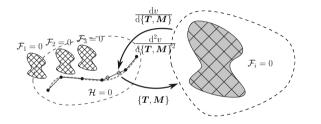
$$\mathcal{H}(\delta\{\epsilon,\beta,\boldsymbol{T},\boldsymbol{M}\},\{\epsilon,\beta,\boldsymbol{T},\boldsymbol{M}\}) = \int_{I} (\delta\epsilon\boldsymbol{T} + \delta\beta\boldsymbol{M} + \delta\boldsymbol{T}\epsilon + \delta\boldsymbol{M}\beta - \delta\boldsymbol{v}) \,\mathrm{d}\boldsymbol{s} - \delta\boldsymbol{L}_{\mathsf{e}} = 0$$

Cross section model: $\mathcal{F}(\delta \hat{\boldsymbol{u}}_i, \hat{\boldsymbol{u}}_i, \{\boldsymbol{T}, \boldsymbol{M}\}) = 0$ compute

$$oldsymbol{v} = \int_{\mathcal{A}} oldsymbol{\mathcal{S}}: oldsymbol{arepsilon} - \psi(oldsymbol{arepsilon},oldsymbol{\chi}) \mathsf{d} oldsymbol{\mathcal{A}}$$

on the cross-section $\mathcal{F} = 0$ with $\{\boldsymbol{T}, \boldsymbol{M}\}$ from beam model

Global model: $\mathcal{H}(\delta{\{\epsilon, \beta, T, M\}}, {\{\epsilon, \beta, T, M\}})$

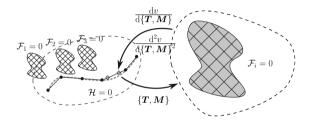


$$\delta \mathbf{v} = \delta \{ \mathbf{T}, \mathbf{M} \} \cdot \frac{\mathrm{d} \mathbf{v}}{\mathrm{d} \{ \mathbf{T}, \mathbf{M} \}}$$

 $\partial \delta \mathbf{v} = \delta \{ \mathbf{T}, \mathbf{M} \} \cdot \frac{\mathrm{d}^2 \mathbf{v}}{\mathrm{d} \{ \mathbf{T}, \mathbf{M} \}^2} \cdot \partial \{ \mathbf{T}, \mathbf{M} \}$



Global model: $\mathcal{H}(\delta\{\epsilon, \beta, T, M\}, \{\epsilon, \beta, T, M\})$

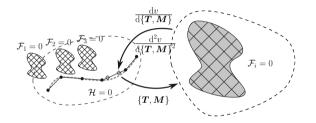


 $\delta \boldsymbol{v} = \delta\{\boldsymbol{T}, \boldsymbol{M}\} \cdot \frac{\mathrm{d}\boldsymbol{v}}{\mathrm{d}\{\boldsymbol{T}, \boldsymbol{M}\}} \qquad \qquad \partial \delta \boldsymbol{v} = \delta\{\boldsymbol{T}, \boldsymbol{M}\} \cdot \frac{\mathrm{d}^2 \boldsymbol{v}}{\mathrm{d}\{\boldsymbol{T}, \boldsymbol{M}\}^2} \cdot \partial\{\boldsymbol{T}, \boldsymbol{M}\}$

Cross section: $\mathcal{F}(\delta \hat{\boldsymbol{u}}_i, \hat{\boldsymbol{u}}_i, \{\boldsymbol{T}, \boldsymbol{M}\}) = 0$

•
$$\frac{dv}{d\{T,M\}}$$
: first order adjoint

Global model: $\mathcal{H}(\delta\{\epsilon, \beta, T, M\}, \{\epsilon, \beta, T, M\})$



$$\delta \boldsymbol{v} = \delta \{ \boldsymbol{T}, \boldsymbol{M} \} \cdot \frac{\mathrm{d} \boldsymbol{v}}{\mathrm{d} \{ \boldsymbol{T}, \boldsymbol{M} \}}$$

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Cross section: $\mathcal{F}(\delta \hat{\boldsymbol{u}}_i, \hat{\boldsymbol{u}}_i, \{\boldsymbol{T}, \boldsymbol{M}\}) = 0$

•
$$\frac{dv}{d\{T,M\}}$$
: first order adjoint

•
$$\frac{d^2v}{d\{T,M\}^2}$$
: second order adjoint

Implementation

```
Cross section:
    class BeamSection():
        # solve the F = 0
        def solve(self, force, moment):
        ....
        # compute the derivative dv/d(T,M)
        def delta_v(self, force, moment):
        ....
        # compute the derivative d<sup>2</sup>v/d<sup>2</sup>(T,M)
        def de_delta_v(self, force, moment):
        ....
```

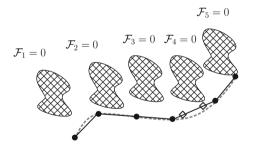


where

solve find the solution of $\mathcal{F} = 0$; delta_v compute the first derivative $\frac{dv}{d\{T,M\}}$ de_delta_v compute the second derivative $\frac{d^2v}{d\{T,M\}^2}$

Implementation

Global beam model $\mathcal{H}=0{:}$ store array beams_sec of BeamSections, one for each cell





Global beam model $\mathcal{H}=0$, array beams_sec



. . .

Global beam model $\mathcal{H} = 0$, array beams_sec

```
class delta_v_expression(UserExpression):
```

```
# evaluate \frac{dv}{d\{T,M\}}
def eval_cell(self, value, x, ufc_cell):
```

```
value = beams_sec[ufc_cell.index].delta_v(self.Tc, self.Mc)
```



Implementation

Global beam model $\mathcal{H} = 0$, class delta_v_expression

$$\int_{I} (\delta \boldsymbol{\epsilon} \boldsymbol{T} + \delta \boldsymbol{\beta} \boldsymbol{M} + \delta \boldsymbol{T} \boldsymbol{\epsilon} + \delta \boldsymbol{M} \boldsymbol{\beta} - \delta \boldsymbol{v}) \, \mathrm{d} \boldsymbol{s} - \delta \boldsymbol{L}_{\boldsymbol{e}}$$

```
# \delta T and \delta M
test_FM = as_vector([v_F[0], v_F[1], ...])
```

```
 \begin{array}{l} \# \ \frac{dv}{d\{\mathcal{T}, M\}} \\ \text{delta}_v = \text{verpr} = \text{delta}_v = \text{verpression}(u, \text{ element} = \text{AZ2\_EL}) \\ \# \ \delta v = \delta\{\mathcal{T}, \mathcal{M}\} \cdot \frac{dv}{d\{\mathcal{T}, \mathcal{M}\}} \\ \text{delta}_v = \text{inner}(\text{test\_FM}, \text{ delta}_v = \text{verpr}) \end{array}
```


Linearization?

Same approach but with
$$\frac{d^2v}{d\{T,M\}^2}$$



Does it work?

Yes



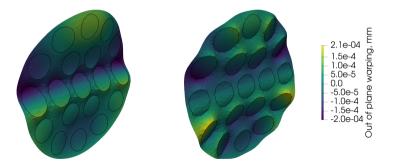
Yes

• quadratic convergence



Yes

- quadratic convergence
- nice results, also with elasto-plastic & hyperelastic materials



Morandini M, A two-level nonlinear beam analysis method, IJSS, 2020



• {**T**, **M**} piece-wise constant discontinuous (DG0)



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- repeated calls, for the same cell, with same $\{\boldsymbol{T}, \boldsymbol{M}\}$



- {**T**, **M**} piece-wise constant discontinuous (DG0)
- repeated calls, for the same cell, with same $\{ \textit{\textbf{T}}, \textit{\textbf{M}} \}$
- \bullet (limited) caching \rightarrow significant speedup



Python Dolfin wrapper

Early in the morning





Python Dolfin wrapper

. . .





Python Dolfin wrapper

...







Python Dolfin wrapper

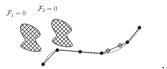
. . .





Python Dolfin wrapper

...



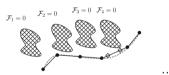
... 20 min ...





Python Dolfin wrapper

. . .

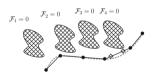


... n x 20 min ...



Python Dolfin wrapper

... late at night



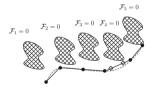
 \dots n x 20 min \dots





Python Dolfin wrapper

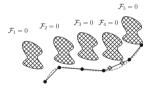
... late at night





Python Dolfin wrapper

... late at night









Why?

• dijitso caches FFC code generation & compilation



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- caching based of Form "signature"



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- Form.signature() gets recomputed!



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Stop-gap solution:



Why?

- dijitso caches FFC code generation & compilation
- caching based of Form "signature"
- Form.signature() really expensive
- Form.signature() gets recomputed!

Stop-gap solution:

replace Form.signature()

hash(.py source file) + form name



Questions/comments?



