Multiscale-in-Time Modeling of Myocardial Growth & Disease Progression

FEniCS conference

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1 Introduction & Motivation

- 2 Modeling the Heart and Disease Mechanisms
- 3 Numerical Implementation using FEniCS-X
- 4 Results
- 5 Summary & Outlook

1.1 Heart Models and the Cardiac Cycle

- Cardiovascular disease entities most prevalent in industrialized world [Dimmeler 2011, Luepker 2011]
- Diseases of the myocardium (heart muscle) are multifactorial and yet to be fully understood
 - Altered mechanical loads
 - > Neurohormonal changes
- Heart may undergo adaptations in structure and shape if loading conditions are chronically above a certain physiological level, referred to as Growth and Remodeling (G & R) [Rossi et al. 1991]
- Volume overload (Fig. (b)):
 - > Heart adapts by eccentric growth (systolic heart failure)
- Pressure overload (Fig. (c)):
 - > Heart adapts by concentric growth (diastolic heart failure)



(a)

RV

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2.1 Patient-specific Geometric 3D-0D Heart Model

 T_{cvcl}

- Pulmonary circulation $C_{\rm cap}^{\rm pul}$ Heart muscle: Nonlinear nearly-incompressible hyperelastic, anisotropic solid [Guccione et al. 1991] $R_{\rm ar}^{\rm pul} L_{\rm ar}^{\rm pul}$ $R_{\rm cap}^{\rm pul}$ $C_{\rm ar}^{\rm pul}$ $\boldsymbol{S} = 2\frac{\partial \Psi}{\partial \boldsymbol{C}} + \underline{\tau_{a}(t)}\boldsymbol{f}_{0} \otimes \boldsymbol{f}_{0} \qquad \Psi = \frac{C_{0}}{2}e^{\boldsymbol{Q}} + \frac{\kappa}{2}(J-1)^{2} \qquad \begin{array}{c} \boldsymbol{Q} = b_{f}E_{ff}^{2} + b_{t}\left(E_{ss}^{2} + E_{nn}^{2} + 2E_{sn}^{2}\right) + \\ + b_{fs}\left(2E_{fs}^{2} + 2E_{fn}^{2}\right) \end{array}$ $Z_{\rm ar}^{\rm pul}$ Contraction: Time- and fiber stretch-dependent active stress law [Bestel et al. 2001] $\tilde{R}^r_{\mathrm{v,ou}}$ $\dot{\tau}_{\mathrm{a}} = -|u|\tau_{\mathrm{a}} + \frac{a\,\sigma_{0}}{|u|_{+}}$ $\dot{a}(\lambda_{\rm mvo}) = \dot{g}(\lambda_{\rm mvo}) \mathbb{I}_{|u|_{-} > 0}$ $\tilde{R}^r_{\rm v,ir}$ $u = \hat{f}(t) \cdot \alpha_{\max} + (1 - \hat{f}(t)) \cdot \alpha_{\min}$ Frank-Starlina mechanism [Solaro 2007] $L_{\rm ven}^{\rm sys}$ p_{y}^{r} $R_{\rm ven}^{\rm sys}$ $oldsymbol{f}_{0}$ |u| > 0+ 2 n $C_{\rm ven}^{\rm sys}$ $n_0 = f_0$ ź .8 1 ĵthres,lo îmax.lo îthres.hi îmax.h
 - Rule-based fiber directions Transmural variation (-60°, 60°) [Doste et al. 2019, Bayer et al. 2012]
- $\begin{array}{c} R_{\text{ven,spl}}^{\text{sys}} & \overrightarrow{R_{\text{ar,spl}}^{\text{sys}}} \\ R_{\text{ven,spl}}^{\text{sys}} & \overrightarrow{R_{\text{ar,spl}}^{\text{sys}}} \\ R_{\text{ven,espl}}^{\text{sys}} & \overrightarrow{R_{\text{ar,spl}}^{\text{sys}}} \\ R_{\text{ven,espl}}^{\text{sys}} & \overrightarrow{R_{\text{ar,spl}}^{\text{sys}}} \\ R_{\text{ven,espl}}^{\text{sys}} & \overrightarrow{R_{\text{ar,spl}}^{\text{sys}}} \\ R_{\text{ven,msc}}^{\text{sys}} & \overrightarrow{R_{\text{ar,spl}}^{\text{sys}}} \\ \end{array} \right)$

• Circulatory system is modeled with a lumped-parameter OD flow model (compliances, resistances inertances) [Hirschvogel et al. 2017, Trenhago et al. 2016, Ursino and Magosso 2000a,b]

 $\lambda_{\rm myo} = \sqrt{f_0 \cdot C f_0}$

Free heart STL geometry from https://www.icmm.ru/tomogram-to-fem

tconti

 t_{relax}

0

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 $C_{\rm ven}^{\rm pul}$

 $\frac{1}{\xi} R_{\rm ven}^{\rm pul}$

 $L_{\rm ven}^{\rm pul}$

 $C_{\mathrm{ar}}^{\mathrm{sys}}$

 $\mathbf{X} R_{\mathrm{ar}}^{\mathrm{sys}}$

 $L_{\rm ar}^{\rm sys}$

2.2 Continuum Mechanical Modeling of G&R

• G&R computed in a kinematic growth framework with multiplicative split of deformation gradient into elastic and inelastic (growth) part [Lee et al. 1969, Rodriguez et al. 1994]

 $\boldsymbol{F}=\boldsymbol{F}^{\mathrm{e}}\boldsymbol{F}^{\mathrm{g}}$

- Growth deformation gradient is function of growth stretch ϑ and possibly of preferred directions \pmb{f}_0 :

$$\pmb{F}^{\mathrm{g}} = f(\vartheta, \pmb{f}_0, \ldots)$$

• Growth stretch usually is governed by an evolution equation and can depend on mechanical or other stimuli:

$$\dot{\vartheta} = f(\vartheta, \boldsymbol{C}, \boldsymbol{S}, \boldsymbol{f}_0, \ldots)$$

• Remodeling is taken into account by additively decomposing the stress response into a part governing the reference and one describing the remodeled material (similar to [Thon et al. 2018]):

 $\boldsymbol{S} = \phi(\vartheta) \boldsymbol{S}_{(\text{remod})} + (1 - \phi(\vartheta)) \boldsymbol{S}_{(\text{base})}$

 $\phi(artheta)$: Fraction of grown material



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3.1 3D-0D Coupled Elastodynamics

- Nonlinear elastodynamics using Generalized-alpha time integration [Chung and Hulbert 1993]
- Strongly coupled 3D-0D monolithic solution of solid mechanics and lumped flow models [Hirschvogel et al. 2017] $\begin{bmatrix} \mathbf{K}^{uu} & \mathbf{K}^{us} \\ \mathbf{K}^{su} & \mathbf{K}^{ss} \end{bmatrix}_{n+1}^{i} \begin{bmatrix} \Delta \mathbf{d} \\ \Delta \mathbf{s} \end{bmatrix}_{n+1}^{i+1} = - \begin{bmatrix} \mathbf{r}^{u} \\ \mathbf{r}^{s} \end{bmatrix}_{n+1}^{i}$
- Use of direct solver (SuperLU) or block-preconditioned GMRES [Elman et al. 2008]
- ~90'000 linear displacement-based tetrahedral elements, ~60'000 unknowns
 - \succ Example healthy heart cycle simulation:





Open-source Python FEniCS-based solver for cardiac mechanics https://github.com/marchirschvogel/ambit

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3.2 Inelastic Deformation-Dependent Growth & Remodeling

- Fiber stretch-driven anisotropic growth in fiber direction $\mathbf{F}^{g} = \mathbf{1} + (\vartheta - 1)\mathbf{f}_{0} \otimes \mathbf{f}_{0} \qquad \dot{\vartheta} = k(\vartheta) \left(\lambda_{myo}^{e} - \hat{\lambda}_{myo}^{crit}\right) \qquad k(\vartheta) = \begin{cases} \frac{1}{\tau} \left(\frac{\vartheta_{max} - \vartheta}{\vartheta_{max} - \vartheta_{min}}\right)^{\gamma}, & \lambda_{myo}^{e} \ge \hat{\lambda}_{myo}^{crit}, \\ \frac{1}{\tau_{rev}} \left(\frac{\vartheta - \vartheta_{min}}{\vartheta_{max} - \vartheta_{min}}\right)^{\gamma}, & \lambda_{myo}^{e} \ge \hat{\lambda}_{myo}^{crit}, \end{cases} \qquad 1.5$
- Stress in inner virtual work depending on deformation and internal variable ϑ , which is deformation-dependent itself in a nonlinear way (needs local Newton to solve) $\delta \mathcal{W}_{int} = \int_{\Omega_0} S(C(u), \vartheta(C(u))) : \frac{1}{2} \delta C \, dV$ Full material tangent expecter reade: $\mathbf{C} = 2 \frac{\partial S}{\partial S} + 2 \left(\frac{\partial S}{\partial S} - \frac{\partial F^g}{\partial S} \right) = \frac{\partial \vartheta}{\partial \theta}$
- Full material tangent operator reads: $\mathbb{C} = 2 \frac{\partial S}{\partial C} + 2 \left(\frac{\partial S}{\partial F^{g}} : \frac{\partial F^{g}}{\partial \vartheta} \right) \otimes \frac{\partial \vartheta}{\partial C}$
 - \succ FEniCS UFL can only take care of first term, since no analytic expressior $\vartheta(C) = ...$ possible
 - $\succ \text{ Express virtual work linearization directly as form without using "derivative" and add second term manually to <math>\mathbb{C}$ $D_{\Delta u} \delta \mathcal{W}_{int} = \int_{\Omega_0} \left(\text{Grad} \delta u : \text{Grad} \Delta u S + F^{\mathrm{T}} \text{Grad} \delta u : \mathbb{C} : F^{\mathrm{T}} \text{Grad} \Delta u \right) dV$ $\frac{\partial S}{\partial F^{\mathrm{g}}} = -\left(F^{\mathrm{g}^{-1}} \overline{\otimes} S + S \underline{\otimes} F^{\mathrm{g}^{-1}} \right) - \left(F^{\mathrm{g}^{-1}} \overline{\otimes} F^{\mathrm{g}^{-1}} \right) : \frac{1}{2} \check{\mathbb{C}}^{\mathrm{e}} : \left(F^{\mathrm{g}^{-\mathrm{T}}} \overline{\otimes} C^{\mathrm{e}} + C^{\mathrm{e}} \underline{\otimes} F^{\mathrm{g}^{-\mathrm{T}}} \right)$ $= \text{Elastic part of } 2\frac{\partial S}{\partial C}$
 - > Depending on growth law, can render excessive FFC-X compilation times! (between 5 and 30 minutes!)

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3.3 Multiscale-in-Time Analysis: Volume Overload and Eccentric Growth in the Heart

- Homeostatic healthy heart beat computation
- Acute disease state (e.g. mitral valve regurgitation) computation, evaluation of end-diastolic volume overload
- Set state "large time scale":

 $\boldsymbol{u}^{(\mathcal{L})} \leftarrow \boldsymbol{u}(t_{\mathrm{ed}})^{(\mathcal{S})} \qquad \hat{p}_c^{i,(\mathcal{L})} \leftarrow p_c^{i,(\mathcal{S})}(t_{\mathrm{ed}}) \qquad \hat{\tau}_{\mathrm{a}}^{(\mathcal{L})} \leftarrow \tau_{\mathrm{a}}(t_{\mathrm{ed}})^{(\mathcal{S})}$

- > Quasi-static growth computation
- Set state "small time scale":

 $\hat{artheta}^{(\mathcal{S})} \leftarrow artheta^{(\mathcal{L})} \qquad oldsymbol{u}^{(\mathcal{S})} \leftarrow oldsymbol{u}^{(\mathcal{L})} - oldsymbol{u}(t_{ ext{ed}})^{(\mathcal{S})}$

- > Compute new homeostatic heat beat state
- Mutually revisit small and large scale until growth falls below a certain tolerance



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4.1 Eccentric Growth in the Heart: Results for Mitral Regurgitation (MR)

- G&R after mitral valve regurgitation
 - Loss of isovolumetric contraction phases
 - Right-shift of pressure-volume relationship
 - > LV wall thinning
 - "Heart failure with reduced ejection fraction"



Acute MR G&R and MR

• Remodeling: Assumption that only active material is reduced with growth (cardiomyocytes are elongated, degradation and disruption of fibrillar collagen, impaired contractility [Aurigemma et al. 2006]):





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5 Summary & Outlook

- Multiphysics and multiscale approach to cardiac growth and remodeling using FeniCS-X
 - > 3D-0D coupled nonlinear elastodynamics and reduced-dimensional flow
 - > Inelastic deformation-dependent growth solved at integration point level
- Physiological results and growth patterns, but ...
 - Need of fine-tuning to match experimental data
- Need for higher-order spatial approximation to avoid spurious effects of low-order finite elements, but ...
 - Missing Quadrature function spaces in FEniCS-X! For linear elements with one integration point (CG1), growth material is specified as discontinuous DG0 function pace
 - > No quadratic convergence for growth material living on DG1 space for higher-order mesh (CG2)
- Need for strategies of reducing FFC-X compiler times for complex constitutive UFL expressions

Thank you for your attention!

References

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